

Optical nanoantenna input impedance

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Supporting Information

S.1 Equation for measurement data fitting

The magnitude of electric field along the transmission line represents a standing wave, which results from the optical wave coupling into the coplanar strip (CPS) from the dipole antenna end and the load antenna end. This superposition was described by a geometric-series expansion to account for all the reflections at the impedance mismatched loads:

$$e_0 = e^{-(\alpha+i\beta)L}, \quad (S1)$$

$$e_1 = e^{-(\alpha+i\beta)(L-x)}, \quad (S2)$$

$$e_2 = e^{-(\alpha+i\beta)x}, \quad (S3)$$

$$E_Z(x) = E_d(e_0 e_1 \Gamma_L + \frac{(e_0^3)(\Gamma_L^2)\Gamma_d e_1}{(1-(e_0^2)\Gamma_d \Gamma_L)} + e_2 + \frac{(e_0^2)\Gamma_L \Gamma_d e_2}{(1-(e_0^2)\Gamma_d \Gamma_L)}) + E_L(e_1 + \frac{(e_0^2)\Gamma_d \Gamma_L e_1}{(1-(e_0^2)\Gamma_d \Gamma_L)} + e_0 e_2 \Gamma_d + \frac{(e_0^3)\Gamma_L(\Gamma_d^2)e_2}{(1-(e_0^2)\Gamma_d \Gamma_L)}) \quad (S4)$$

where Γ_L is the reflection coefficient at the load terminal (for example: a folded dipole), and Γ_d is the reflection at the single dipole terminal. Γ_d is determined in two ways; 1) using a lumped-port excitation, and 2) by fitting the standing wave on a CPS loaded with identical dipoles on either end, with good agreement and with values validated against prior results in reference [25]. E_d and E_L are the magnitude at dipole side and load side. L is the length of the transmission line. The origin is at the dipole end ($x=0$) similar to the paper. The attenuation constant α was extracted from the decaying complex field amplitude as a function of position along an electrically long CPS predicted

through full-wave analysis and the phase constant β was determined from the spatial periodicity in the wave function, respectively:

$$\beta = \frac{2\pi}{\lambda} \quad (S5)$$

$$\alpha = \frac{20 \log_{10}(E1/E2)}{8.69d} \quad (S6)$$

where d is the distance between $E1$ and $E2$. The attenuation and phase constant should be averaged by calculating through the whole length of CPS.

The impedance of the antenna under test (AUT) was determined from the reflection coefficient, Γ_L , expressed as:

$$Z_L = \left(\frac{1+\Gamma_L}{1-\Gamma_L}\right)Z_0 \quad (S7)$$

where Z_0 is the characteristic impedance of the CPS, Γ_L is the reflection coefficient at the load terminal which was determined from the fitting equation (S4) and Z_L is the impedance of the load antenna.

The characteristic impedance of CPS, which exhibits a high confinement associated with transmission mode here, was determined by changing the open-circuit and short-circuit load with expression:

$$Z_{in} = Z_0 \left(\frac{Z_L \cosh(\gamma L) + Z_0 \sinh(\gamma L)}{Z_0 \cosh(\gamma L) + Z_L \sinh(\gamma L)}\right) \quad (S8)$$

where L is the length of CPS, $\gamma = \alpha + j\beta$, Z_L is load impedance and Z_0 is input impedance of CPS. In the open-circuit mode operation, Z_L goes to a very large number, $Z_{oc} = Z_0 \left(\frac{\cosh(\gamma L)}{\sinh(\gamma L)}\right)$, while in the short-circuit mode operation, Z_L equals zero, $Z_{sc} = Z_0 \left(\frac{\sinh(\gamma L)}{\cosh(\gamma L)}\right)$. The input impedance of CPS can be achieved from following:

$$Z_0 = \sqrt{(Z_{sc}Z_{oc})} \quad (S9)$$

where Z_{sc} is the input impedance when Z_L is a short-circuit load and Z_{oc} is the input impedance when Z_L is an open-circuit load.

S.2 Numerical method of driven model in HFSS

Ansys high frequency structural simulator (HFSS) is a commercial finite element method solver for electromagnetic structures (<http://www.ansys.com>). The driven model in HFSS was implemented to compute the input impedance of nanoantennas directly, by driving the nanoantenna at its feed gap with an optical source. Antenna impedance, Z_A , can be defined as the ratio of the effective voltage across the antenna arms and the optical displacement current flowing through the gap. Fig. S1 gives an example of feed-gap excitation for the folded dipole antenna in HFSS.

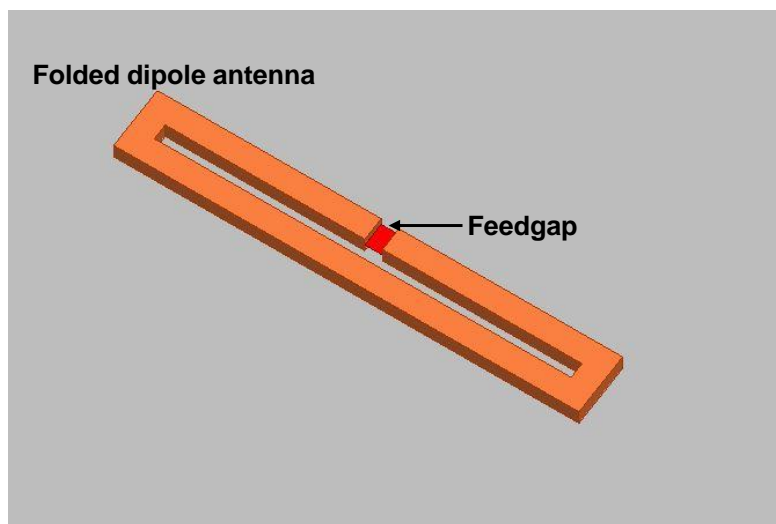


Figure S1| Folded dipole antenna with a feed gap excitation in HFSS

S.3 Analytical fitting to the measured data of double-folded and triple-folded dipole antennas

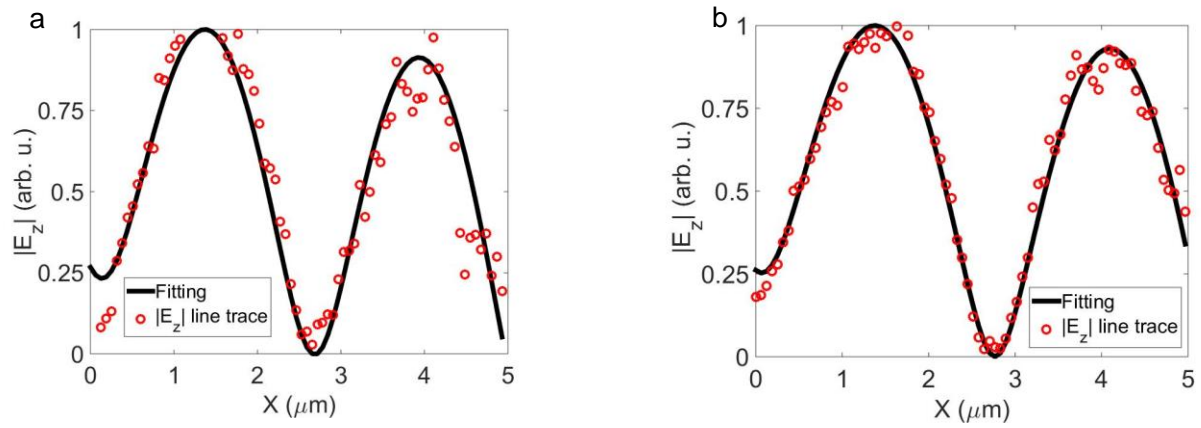


Figure S2| Analytical fitting to the measured data for the (a) doubled- and (b) triple-folded dipole antennas